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# MHD FLOW OF A NANOFLUID AT THE FORWARD STAGNATION POINT OF AN INFINITE PERMEABLE WALL WITH A CONVECTIVE BOUNDARY CONDITION

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#### ABSTRACT

The steady magnetohydrodynamic (MHD) flow of a nanofluid at the forward stagnation point of an infinite permeable wall is investigated in this study. A mathematical model has been constructed and the governing partial differential equations are converted into ordinary differential equations by similarity transformation. The similarity equations are solved numerically by a shooting technique. Results for the surface shear stresses, surface heat transfer, and velocity, nanoparticle fraction and temperature profiles are presented in tables and in some graphs. Effects of the magnetic parameter, constant mass flux Biot number, Brownion motion parameter thermophoresis parameter and Lewis number are examined. The present results are compared with previously available numerical results obtained using other methods of solution, and they are found to be in good agreement.

Keywords: MHD flow, Nanofluid, Stagnation point, Infinite permeable wall, Numerical solution.

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## **Contribution/ Originality**

This study documents important features of MHD stagnation point flow with the effect of convective boundary condition also suction and injection. The paper's contribution is finding that the development of skin friction, heat flux and mass flux, with the velocity, temperature and nanoparticle fraction profiles, in tables and graphs.

#### Nomenclature

- a constant
- $B_0$  magnetic field normal to the wall
- Bi Biot number
- C constant nanoparticle fraction
- $C_f$  skin friction coefficient

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$C_p$	specific heat at constant pressure
$C_{_{W}}$	constant wall nanoparticle fraction
$C_{\infty}$	constant nanoparticle fraction (inviscid flow)
$D_{\scriptscriptstyle B}$	Brownian diffusion coefficient
$D_T$	thermophoresis diffusion coefficient
$h_{_f}$	convective heat transfer coefficient
k	thermal conductivity
Le	Lewis number
М	magnetic parameter
Nh	Brownion motion parameter
N+	
111	thermophoresis parameter
$Nu_x$	localNusselt number
Pr	Prandtl number
$q_{\scriptscriptstyle m}$	mass flux
$q_{_{W}}$	heat flux
Re <sub>x</sub>	local Reynolds number
S	constant mass flux
$Sh_x$	local Sherwood number
Т	constant temperature
$T_{f}$	convective fluid temperature below the surface of the wall
$T_w$	temperature of the surface of the wall
$T_{\infty}$	constant temperature (inviscid flow)
u,v	velocity component in the $x$ and $y$ direction, respectively
И <sub>е</sub>	external stream (inviscid flow)
$\mathcal{V}_w$	mass flux velocity
<i>x</i> , <i>y</i>	Cartesian coordinates along the surface and normal to it, respectively

fluid

α	thermal diffusivity					
$\eta$	pseudo-similarity variable					
$\varphi$	solid volume fraction of the nanofluid					
ρ	density					
$\sigma$	electric conductivity					
$\theta$	dimensionless temperature					
τ	ratio between the effective heat capacity of nanoparticle and heat capacity of the					
$ au_{_W}$	skin friction or shear stress					
ν	kinematic viscosity					
Ψ	stream function					
$(\rho C_p)$	$f_f$ heat capacity of the fluid					
$(\rho C_p)$	$p_p$ heat capacity of the nanoparticle material					
Superscr	ipt					
,	differentiation with respect to $\eta$					
Subscrip	t					

W	condition at the wall
$\infty$	condition at infinity

## 1. INTRODUCTION

The flow near the stagnation point has attracted the attention of many investigators for many years because of its wide applications both in industrial and scientific applications. Some of the applications are cooling of electronic devices by fans, solar central receivers exposed to wind currents, and many hydrodynamic processes in engineering applications. The study of two dimensional stagnation point flows towards a solid surface in moving fluid was first studied by Hiemenz [1] in 1911 and follows by Homann [2] for the axissymmetric stagnation point flow. Many researchers have been working still on the stagnation point flows in various way. Mahapatra and Gupta [3] extended the stagnation point study by considering a stretching surface. Moreover, the stagnation point flow of a micropolar fluid towards stretching sheet was studied by Nazar [4] etc.

The problem of MHD flow at the stagnation point is a thoroughly researched problem in fluid mechanics. The steady MHD mixed convection flow near the stagnation point on a vertical permeable surface has been examined by Ishak [5] and they found that dual solutions are exist for both assisting and opposing cases. Mahapatra, et al. [6]; Ray Mahapatra, et al. [7] investigated two dimensional MHD stagnation point flow of a power law fluid towards a stretching surface numerically and analytically.

In recent years, some interest has been given to the study of convective transport of nanofluids. The theory of nanofluid first introduced by Choi and Eastman [8] and has been a field of very active research area. Kuznetsov and Nield [9] examined the influence of nanoparticles on natural convection flow past a vertical flat plate, using a model in which Brownion motion and thermophoresis are accounted for. They found that the reduced Nusselt

number is a decreasing function of Brownion motion and thermophoresis parameter. Then, Khan and Pop [10] formulated the problem of laminar boundary layer flow of a nanofluid past a stretching sheet and Mustafa [11] considering the flow at the stagnation point for nanofluid towards a stretching sheet. The problem of boundary layer flow of a nanofluid past a stretching sheet has been investigated analytically by using the Homotopy Analysis Method by Hassani [12]. This work was extended by Bachok, et al. [13] by taking an account of shrinking case and discover a non-unique solution. Further, they continue the research by considering an unsteady flow and permeable sheet (see Bachok, et al. [14]). Ibrahim, et al. [15] analyzed the effect of magnetic field on stagnation point flow and heat transfer due to nanofluid towards a stretching sheet. There are many other studies have been conducted which relates to nanofluids such as Khan and Aziz [16]; Alsaedi, et al. [17]; Aziz and Khan [18]; Hamad and Ferdows [19] and Rana and Bhargava [20].

There has been considerable interest also in flows past permeable walls with suction and injection. The process of suction and injection has its importance in many engineering applications such as in the design of thrust bearing and radial diffusers, and thermal oil recovery. Suction is applied to chemical processes to remove reactants while injection is used to add reactants, cool the surfaces, prevent corrosion or scaling and reduce the drag (see Labropulu, et al. [21]). Katagiri [22] investigated the behavior of magnetohydrodynamic flow with suction or injection at the forward stagnation point and solved numerically. Kandasamy, et al. [23] explored the problem of MHD boundary layer flow of a nanofluid past a vertical stretching surface in the presence of suction and injection. Then, Ibrahim and Shankar [24] extended the study by took into account the slip boundary condition past a permeable stretching sheet. The same boundary layer flow of nanofluid also been investigated for semi infinite flat plate by Hamad, et al. [25]. Recently, the influenced of nanoparticles on mixed convection boundary layer flow along an inclined surface in a porous medium with Brownion motion and thermophoresis effect were examined by Rana, et al. [26]. The similarity solutions to the convective heat transfer problems have been studied by Aziz [27] and Magyari [28] for an impermeable plate, and by Ishak [29] for a permeable plate.

Recently, there are studies of heat transfer problem for boundary layer flow that put convective boundary condition into account. Aziz [27] discussed on the similarity solution of thermal boundary layer over a flat plate and then Ishak [29] extends it by considering the effect of suction and injection. The effect of convective boundary condition in nanofluid also have been investigated by Makinde, et al. [30] with internal heat generation/absorption and followed by Alsaedi, et al. [17] with analysis of stagnation point flow. An effect of stretching and shrinking with convective boundary condition was analyzed by Bachok, et al. [31] and Nandy and Mahapatra [32]. Recently, Akbar [33] and Hamad, et al. [34] conducted a study of MHD stagnation point flow undet convective boundary condition with radiation effects. It is worth mentioning that many other boundary layer problems with convective boundary condition were investigated by Merkin and Pop [35]; Rashad, et al. [36]; Makinde and Aziz [37]; Makinde and Aziz [38] and Makinde, et al. [39].

Motivated by the above investigations, the present paper deals with the problem of steady MHD boundary layer flow and heat transfer and nanoparticle fraction over a two-dimensional stagnation point on an infinite permeable wall with convective boundary condition. We also investigate the effect of suction and injection on the system. The governing partial differential equations are first transformed into ordinary differential equations using similarity transformation, before being solved numerically by using shooting technique. The numerical results obtained are then compared with the data available in the literature for certain particular cases of the problem, to support their validity.

# 2. BASIC EQUATIONS

Consider the steady two-dimensional laminar flow of an incompressible and viscous nanofluid at the forward stagnation point of an infinite permeable wall, which is assumed to be an electric insulator. It is assumed that the velocity of the external stream (inviscid flow) is  $u_e(x) = ax$ , where a is a positive the constant, and  $v_w$  is the mass flux velocity, where  $v_w < 0$  corresponds to suction and  $v_w > 0$  corresponds to injection, respectively. Then, we assume that the constant temperature T and the constant nanoparticle fraction C in the ambient fluid (inviscid flow) are denoted by  $T_{\infty}$  and  $C_{\infty}$ , respectively. A uniform magnetic field  $B_0$  is applied normal to the wall. The nanofluid is assumed to have constant properties. In addition, the assumptions of small magnetic Reynolds number and of zero electric field have been made. Cartesian coordinates x and y are measured along the wall and perpendicular to it, respectively, as shown in Figure 1.



Figure-1. Physical model and coordinate system

Under these assumptions, the basic boundary layer equations of conservation of mass, momentum, thermal energy and nanoparticle fraction can be written as, see Kuznetsov and Nield [9] and Katagiri [22].

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0 \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = u_e \frac{d u_e}{d x} + v \frac{\partial^2 u}{\partial y^2} + \frac{\sigma B_0^2}{\rho} (u_e - u)$$
(2)

$$u\frac{\partial T}{\partial x} + v\frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial y^2} + \tau \left[ D_B \frac{\partial T}{\partial y} \frac{\partial C}{\partial y} + \frac{D_T}{T_{\infty}} \left( \frac{\partial T}{\partial y} \right)^2 \right]$$
(3)

$$u\frac{\partial C}{\partial x} + v\frac{\partial C}{\partial y} = D_B \frac{\partial^2 C}{\partial y^2} + \frac{D_T}{T_\infty} \frac{\partial^2 T}{\partial y^2}$$
(4)

where u and v are the velocity component in the x and y directions, v is the kinematic viscosity,  $\alpha$  is the thermal diffusivity of the nanofluid,  $\rho$  is the density,  $\sigma$  is the electric conductivity,  $D_B$  is the Brownian diffusion

coefficient,  $D_T$  is the thermophoresis diffusion coefficient and  $\tau$  is the ratio between the effective heat capacity of the nanoparticle material and heat capacity of the fluid,  $\tau = (\rho C_p)_p / (\rho C_p)_f$ ,  $C_p$  being the specific heat at constant pressure.

Following Aziz [27] and Ishak [29] we assume that the temperature of the surface of the wall is maintained by convective heat transfer at a certain value  $T_w$ , which is to be determined later. Thus, the boundary conditions of Eqs. (1) - (4) are

$$v = v_w, \quad u = 0, \quad -k \frac{\partial T}{\partial y} = h_f \left( T_f - T_w \right), \quad C = C_w \quad \text{at} \quad y = 0$$

$$u \to u_e, \quad T \to T_\infty, \quad C \to C_\infty \quad \text{as} \quad y \to \infty$$
(5)

Where k is the thermal conductivity,  $T_f$  is the convective fluid temperature below the surface of the wall,  $h_f$  is the convective heat transfer coefficient and  $C_w$  is the constant wall nanoparticle fraction.

We look for a similarity solution of Eqs. (1)to (4), with the boundary conditions (5) of the following form

$$\psi = (\nu a)^{1/2} x f(\eta), \quad \theta(\eta) = \frac{T - T_{\infty}}{T_w - T_{\infty}}, \quad \varphi(\eta) = \frac{C - C_{\infty}}{C_w - C_{\infty}}, \quad \eta = \left(\frac{a}{\nu}\right)^{1/2} y \tag{6}$$

where  $\psi$  is the stream function, which is defined as  $\mathbf{u} = \partial \psi / \partial \mathbf{y}$  and  $\mathbf{v} = -\partial \psi / \partial \mathbf{x}$ . Thus, we have

$$u = a x f'(\eta), \quad v = -(a v)^{1/2} f(\eta)$$
 (7)

where primes denote differentiation with respect to  $\eta$ . Therefore, in order that Eqs. (1) - (4) have a similarity solution, we take

$$v_w = -\left(a\,v\right)^{1/2}s\tag{8}$$

where s is the constant mass flux where s > 0 corresponds for suction and s < 0 correspond for injection, respectively.

Substituting (7) into Eqs.(2) to (4), we obtain the following ordinary differential equations

$$f''' + f f'' + 1 - f'^{2} + M(1 - f') = 0$$
<sup>(9)</sup>

$$\frac{1}{\Pr}\theta'' + f\theta' + Nb\theta'\varphi' + Nt(\theta')^2 = 0$$
<sup>(10)</sup>

$$\varphi'' + Le f \varphi' + \frac{Nt}{Nb} \theta'' = 0 \tag{11}$$

and the boundary conditions (5) become

$$f(0) = s, \quad f'(0) = 0, \quad \theta'(0) = -Bi[1 - \theta(0)], \quad \varphi(0) = 1$$
  
$$f'(\eta) \to 1, \quad \theta(\eta) \to 0, \quad \varphi(\eta) \to 0 \quad \text{as} \quad \eta \to \infty$$
(12)

Where  $\Pr = v/\alpha$  is the Prandtl number and  $\operatorname{Le} = v/\operatorname{D}_{B}$  is the Lewis number. Further, M is the magnetic parameter, Bi is the Biot number, Nb is the Brownian motion parameter and Nt is the thermophoresis parameter, which are defined as

$$M = \frac{\sigma B_0^2}{\rho a}, \quad Bi = \frac{h_f}{k} \left(\frac{a}{\nu}\right)^{1/2}, \quad Nb = \frac{\tau D_B \left(C_w - C_\omega\right)}{\nu}, \quad Nt = \frac{\tau D_T \left(T_w - T_\omega\right)}{\nu T_\omega}$$
(13)

Quantities of physical interest are the skin friction coefficients  $C_f$ , the local Nusselt number  $Nu_x$  and the local

Sherwood number  $\mathit{Sh}_x$ , which can be expressed as

$$C_{f} = \frac{\tau_{w}}{\rho u_{e}^{2}}, \quad Nu_{x} = \frac{x q_{w}}{k \left(T_{w} - T_{\infty}\right)}, \quad Sh_{x} = \frac{x q_{m}}{D_{B} \left(C_{w} - C_{\infty}\right)}$$
(14)

where  $\tau_w$  is the skin friction or shear stress and,  $q_w$  and  $q_m$  are the heat flux and the mass flux, respectively, from the surface of the sheet, which are defined as

$$\tau_{w} = -\mu \left(\frac{\partial u}{\partial y}\right)_{y=0}, \quad q_{w} = -k \left(\frac{\partial T}{\partial y}\right)_{y=0}, \quad q_{m} = -D_{B} \left(\frac{\partial C}{\partial y}\right)_{y=0}$$
(15)

Substituting (6) into (15) and using (14), we obtain

$$\operatorname{Re}_{x}^{1/2} C_{f} = f''(0), \quad \operatorname{Re}_{x}^{-1/2} Nu_{x} = -\theta'(0), \quad \operatorname{Re}_{x}^{-1/2} Sh_{x} = -\varphi'(0)$$
(16)

where  $\operatorname{Re}_{x} = u_{e}(x) x / v$  is the local Reynolds numbers.

It is worth mentioning that when Bi = 0, the lower side of the wall with hot fluid is totally insulated and no convective heat transfer to the cold fluid upwards of the wall takes place. Further, it should be noticed at this end that the solution of the energy equation (10) approaches the solution of the constant surface temperature

$$\theta(0) = 1 \text{ as } Bi \to \infty$$
.

#### 3. RESULTS AND DISCUSSION

The ordinary differential equations (9) to (11) subject to the boundary condition (12) have been solved numerically for some values of the governing parameters M, s, Bi, Nb, Nt and Le using a shooting method. The value of the Prandtl number is taken  $\Pr = 1$  throughout this paper. In addition, we also interested to look on some physical quantities which were skin friction coefficient, f''(0), the heat flux  $-\theta'(0)$  and mass flux  $-\phi'(0)$ .

The obtained results for the skin friction coefficient f''(0), for various values of the parameter M and s have been compared with those reported by Katagiri [22] and were shown in Table 1. Note that this is for the case of no energy and no concentration equation. From this table, we noticed that the comparison shows a very good agreement for each value of f''(0),  $-\theta'(0)$  and  $-\phi'(0)$ . This comparison lends confidence in the numerical results to be reported in the next table for several values of Le and Bi for both suction and injection cases. By referring Table 2, it shows that the values of f''(0) were independent of Le and Bi. The values of  $-\theta'(0)$ and  $-\phi'(0)$  decrease as Le and Bi increase except for  $-\phi'(0)$  in suction case where it increase when Leincrease.

Fig. 2 shows the effects of s and M on f''(0) graphically. From this figure, it shows that as both parameter M and s increase, the values of f''(0) also increase. The same results also have been agreed by Katagiri [22] for impermeable case. From Fig. 3, as Nt increase from 0 to 0.6, the values of  $-\theta'(0)$  decrease for both suction and injection cases. Similar result have been observed by Aziz and Khan [18]. The graph also illustrate that when Nb increase,  $-\theta'(0)$  decrease for both suction and injection cases. The variation of  $-\phi'(0)$ as Nt increase have been shown at Fig. 4. We can see clear difference for both suction and injection cases where along with an increment of Nt value, the value of  $-\phi'(0)$  decrease for suction case but increase for injection case. The graph also explain the changes of  $-\phi'(0)$  as Nb increase. From Fig. 4(a), we noticed that the value of  $-\phi'(0)$  increase when Nb increase while  $-\phi'(0)$  decrease when Nb increase for injection case which shown at Fig. 4(b).

Next, we can see the variation of  $-\phi'(0)$  for different values of Lewis number, Le and Biot number, Bi from Fig. 5. The value of  $-\phi'(0)$  increase for suction case while decrease for injection case when the value of Lewis number, Le increase. Fig. 5 (a) illustrate that  $-\phi'(0)$  was slightly decrease at the beginning as Bi increase. Whilst, a slight increase of  $-\phi'(0)$  at Bi < 1 can be seen in Fig. 5(b) when Bi increase.

Fig. 6 to 9 illustrate the effects of parameter M, s, Nb and Bi on velocity profile  $f'(\eta)$ , temperature profile  $\theta(\eta)$  and nanoparticle fraction profiles  $\phi(\eta)$ . These profiles satisfy the far field boundary conditions (12) asymptotically, which support the validity of numerical solution obtained. For Fig. 6, it shows the effects of M on each profiles where the solid line refers to suction case and broken line refers to injection case. By referring to Fig. 6(a), when the value of M increase, the velocity also increase for both suction and injection cases. Fig. 6(b) explains that the temperature of the system decrease when M increase. The same trend can be found in Fig. 6(c), where the nanoparticle fraction decrease when M increase for both cases. In addition, we also can see that there are small influence of M on temperature and nanoparticle profiles for suction case compared to injection case by referring on Fig. 6(b) and (c). Fig. 7 shows the effects of s on each profiles. From Fig. 7(a), it explained that the velocity of the system are increase together with s which also obtained by Katagiri [22] for impermeable case. However, contrary to the present observation, Ishak [5] and Bachok, et al. [14] found that as s increase, the velocity decrease for regular fluid and nanofluid, respectively. Besides, the temperature and nanoparticle fraction are decreased with s which can be seen in Fig. 8(b) and (c), and Bachok, et al. [14] also reported the similar result. We also noticed that the graph shape is still the same from the value of suction to injection.

Fig. 8 illustrate the temperature profiles with the change of Brownion motion parameter, Nb. From Fig. 8 (a), it shows that the temperature increase with Nb for both suction and injection cases. A slight different of trend can be seen for nanoparticle fraction when suction and injection (see Fig. 8(b)). For suction case, we can see that nanoparticle fraction decrease when Nb increase.

Effects of Biot number Bi on temperature profiles can be seen in Fig. 9. It shows that both temperature for suction and injection cases are increase together with the value of Bi. Furthermore, the higher the Bi, the closer the value of  $\theta(0)$  approaching 1 at the boundary. This can be proved from the boundary condition (12) which reduces to  $\theta(0)=1$  if  $Bi \rightarrow \infty$ . Aziz [27] noted the same pattern for the temperature profiles.

M	S	Katagiri [22] $f''(0)$	Present Results
			f''(0)
1	-1	1.116421	1.116421
	-0.5	1.331153	1.331154
	0	1.585327	1.585331
	0.5	1.877166	1.877176
	1	2.20292	2.202940
	1.5	2.557898	2.557937
	2	2.937316	2.937384
	2.5	3.336797	3.336905
	3	3.752586	3.752749
2	-1	1.405659	1.405659
	-0.5	1.622920	1.622924
	0	1.873519	1.873527
	0.5	2.156606	2.156623
	1	2.469924	2.469955
	1.5	2.810327	2.810379
	2	3.174309	3.174391
	2.5	3.558404	3.558527
	3	3.959429	3.959605

Table-1.Comparison of results for the values of f''(0) for several values of M and s .

Table-2. Values of f''(0),  $-\theta'(0)$  and  $-\phi'(0)$  for several values of Bi when M=1, s=1 (suction), s=-1

S	Le	Bi	f''(0)	- heta'(0)	$-\phi'(0)$
1	1	0.1	2.202940	0.910438	1.275161
		0.5	2.202940	0.661393	1.113066
		1.0	2.202940	0.487094	1.010323
		5.0	2.202940	0.152556	0.836141
		10.0	2.202940	0.081723	0.802935

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	5	0.1	2.202940	0.897044	5.195860
		0.5	2.202940	0.621653	5.073030
		1.0	2.202940	0.441633	5.005761
		5.0	2.202940	0.129098	4.910766
		10.0	2.202940	0.068203	4.895214
	10	0.1	2.202940	0.893047	10.11542
		0.5	2.202940	0.610363	10.00105
		1.0	2.202940	0.429316	9.941435
		5.0	2.202940	0.12335	9.86200
		10.0	2.202940	0.064957	9.849624
-1	1	0.1	1.116421	0.490115	0.189373
		0.5	1.116421	0.151282	0.222413
		1.0	1.116421	0.080664	0.229284
		5.0	1.116421	0.017009	0.235469
		10.0	1.116421	0.008562	0.236289
	5	0.1	1.116421	0.482957	0.017123
		0.5	1.116421	0.147208	0.024405
		1.0	1.116421	0.078291	0.025803
		5.0	1.116421	0.016472	0.027030
		10.0	1.116421	0.008289	0.027191
	10	0.1	1.116421	0.482478	0.005580
		0.5	1.116421	0.146969	0.008633
		1.0	1.116421	0.078156	0.009209
		5.0	1.116421	0.016442	0.009713
		10.0	1.116421	0.008274	0.009779



Fig-2. Variation of f''(0) with M for several values of swhen Nb = 0.5, Nt = 0.5, Le = 10 and Bi = 1.



Fig-3. Variation of  $-\theta'(0)$  with Nt for several values of Nb when M = 1, Le = 10 and Bi = 1 for (a) suction and (b) injection case



Fig-4. Variation of  $-\phi'(0)$  with Nt for several values of Nb when M = 1, Le = 10 and Bi = 1 for (a) suction and (b) injection case



Fig-5. Variation of  $-\phi'(0)$  with Bi for several values of Le when M = 1, Nb = 0.5, Nt = 0.5 and Bi = 1 for (a) suction and (b) injection case



Fig-6. Effects of M on the (a) velocity profile  $f'(\eta)$ , (b) temperature profile  $\theta(\eta)$  and (c) nanoparticle fraction profiles  $\phi(\eta)$  when Nb = 0.5, Nt = 0.5, Le = 10 and Bi = 1 for both suction (s = 1) and injection (s = -1) cases.



Fig-7. Effects of *S* on the (a) velocity profile  $f'(\eta)$ , (b) temperature profile  $\theta(\eta)$  and (c) nanoparticle fraction profiles  $\phi(\eta)$  when Nb = 0.5, Nt = 0.5, Le = 10 and Bi = 1.



Fig-8. Effects of Nb on the (a) temperature profile  $\theta(\eta)$  and (b) nanoparticle fraction profiles  $\phi(\eta)$  when M = 1, Nt = 0.5, Le = 10 and Bi = 1 for both suction (s = 1) and injection (s = -1) cases.



Fig-9. Effects of Bi on the temperature profile  $\theta(\eta)$  when M = 1, Nt = 0.5, Nb = 0.5 and Le = 10 for both suction (s = 1) and injection (s = -1) cases.

## 4. CONCLUSION

We have theoretically investigated the effects of various governing parameters magnetic parameter M, constant suction/injection parameter s, Brownian motion parameter Nb, thermophoresis parameter Nt, Biot number Bi and Lewis number Le on flow field and heat transfer characteristics of the MHD stagnation point flow of a nanofluid at the forward stagnation point of an infinite permeable wall. The numerical results obtained are in excellent agreement with the previously published data available. It is found that the magnitude of skin friction

f''(0), the local Nusselt number  $-\theta'(0)$  and the local Sherwood number  $-\phi'(0)$  all are increasing with M and

s.

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